## Lect 6

Image Theory.

Arrays of two isotropic point sources.

## Image Theory

Vertical Electric Dipole (VED)


Virtual source
(image)
Copyright © 2005 by Constantine A. Balanis All rights reserved

Fig. 4.12a
Chapter 4
Linear Wire Antennas

## Actual and Equivalent Problems



## Actual Problem

Copyright© 2005 by Constantine A. Balanis All rights reserved

## Equivalent Problem

Chapter 4
Linear Wire Antennas

## Electric conductor


vertical dipole above infinite ground plane

vertical dipole above infinite ground plane

$$
\begin{aligned}
& E_{\theta}=j \eta \frac{k I_{o} l e^{-j k r_{1}}}{4 \pi r} \sin \theta+j \eta \frac{k I_{o} l e^{-j k r_{2}}}{4 \pi r} \sin \theta \\
& E_{\theta}=j \eta \frac{k I_{o} l e^{-j k r}}{4 \pi r} \sin \theta\left[e^{j k h \cos \theta}+e^{-j k h \cos \theta}\right] \\
& E_{\theta}=j \eta \frac{k I_{o} l e^{-j k r}}{4 \pi r} \sin \theta[2 \cos (k h \cos \theta)] \quad z \geqslant 0 \\
& E_{\theta}=0
\end{aligned} \quad z<0
$$



Copyright© 2005 by Constantine A. Balanis All rights reserved

Chapter 4
Linear Wire Antennas

## Scalloping Of Amplitude Pattern Of Vertical Dipole

$\theta \longleftrightarrow \downarrow$


## Horizontal Dipole



Horizontal dipole above infinite ground plane


## Horizontal dipole above infinite ground plane

$$
\begin{aligned}
& =j \eta \frac{k I_{o} l e^{-j k r_{1}}}{4 \pi r} \sqrt{1-\sin ^{2} \theta \sin ^{2} \phi}-j \eta \frac{k I_{o} l e^{-j k r_{2}}}{4 \pi r} \sqrt{1-\sin ^{2} \theta \sin ^{2} \phi} \\
E_{\psi} & =j \eta \frac{k I_{o} l e^{-j k r}}{4 \pi r} \sqrt{1-\sin ^{2} \theta \sin ^{2} \phi}\left[e^{j k h \cos \theta}-e^{-j k h \cos \theta}\right] \\
E_{\psi} & =j \eta \frac{k I_{o} l e^{-j k r}}{4 \pi r} \sqrt{1-\sin ^{2} \theta \sin ^{2} \phi}[2 j \sin (k h \cos \theta)] \quad \mathrm{z} \geqslant 0 \\
E_{\psi} & =0
\end{aligned}
$$

An infinitesimal dipole of length $1=\lambda / 50$ is placed vertically above the ground at height $\mathrm{h}=2 \lambda$ Derive an equation for its field pattern


Example (Problem 4.37)
Determine the smallest height that an infinitesimal vertical electrical dipole of $\mathrm{l}=\lambda / 50$ must be placed above an Electrical ground plane so that AF Pattern has only one null at $30^{\circ}$ from The vertical. For that height find -The directivity -the radiation resistance

$$
\begin{aligned}
& \text { nullat } w^{\circ} \text { 8-r the Ar.iy Factor, AF }=\cos (k h \cos \theta)
\end{aligned}
$$

$$
\begin{aligned}
& \text { bot mull }=30 \text { and au .... son.. } \\
& \frac{2 \pi}{\lambda} h \cos 30=\frac{\pi}{2} \\
& \therefore h=\frac{\lambda}{2 \sqrt{s}} \rightarrow k h=\frac{2 \pi}{\lambda} \frac{\lambda}{2 \sqrt{3}}=\frac{\pi}{\sqrt{3}} \\
& \text { Max Difectivity } D=\frac{4 \pi}{\sqrt{2}} \quad \Omega=\int_{0}^{2 \pi} \int_{0}^{\pi / 2} \sin \theta d \theta \partial \phi \\
& D=\frac{2}{\int^{2} \sin ^{3} \theta \cos ^{2}\left(\frac{\pi}{\sqrt{3}} \cos \theta\right) d \theta} \\
& =\frac{2}{0.39}=511 \frac{1-1 y}{}=7.12 B \\
& \left.\therefore|E|=7 \frac{K Q I}{2 \pi r} \sin \theta \cos (x h \cos \theta) \quad \geq 1 s=\frac{1}{2 \eta} \right\rvert\, E I^{2} \alpha r \\
& \therefore \omega=\frac{1}{2 \eta} \eta^{2}\left(\frac{2 \pi}{\lambda} \frac{\lambda}{50} \frac{1}{2 \pi}\right)^{2} J_{0}^{2} \sin ^{2} \theta \cos ^{2}(k h \cos \theta) \\
& \text { Rad }=\frac{1}{2} I_{0}^{2} R_{r}=\int_{0}^{2 \pi} \int_{0}^{\pi / 2} U d \Omega \\
& =\frac{1}{2} I_{0}^{2} R_{r}=2 \pi \frac{1}{2} \eta\left(\frac{1}{50}\right)^{2} I_{0}^{2} \int_{0}^{\pi / 2} \sin ^{2} \theta \cdot \cos ^{2}(k h \cos \theta) d \theta \\
& R_{r}=\frac{2 \pi \times 120 \pi}{(50)^{2}} \times 0.39=0.369 \Omega
\end{aligned}
$$

A doublet of length $\mathrm{L}=\lambda / 50$ is place horizontally above the ground at a height $\mathrm{h}=2 \lambda$.
Derive an equation for its field pattern.

## Solution:


$\therefore E=E_{1}+E_{2}$
$=j \frac{z_{0}}{2} \frac{I d l}{r_{1} \lambda} \sin \left(\frac{\pi}{2}-\theta\right) e^{-j \sigma_{1}}-j \frac{z_{c}}{2} \frac{I d t}{\lambda r_{2}} \sin \left(\frac{\pi}{2}-\theta\right) e^{-j k_{1}}$
$=j \frac{z_{0}}{2} I \frac{d t}{\lambda}\left[\frac{e^{-j k_{1}}}{r_{1}}-\frac{e^{-j k_{r_{1}}}}{r_{2}}\right] \operatorname{Cos}(\theta)$
$r_{1} \cong r-h \cos \theta$
$r_{2} \cong r+h \cos \theta$
As in the for field zone: wing $r_{1} \& r_{2}$ is approx. the same as using $r$ when found in the denominator

$$
\begin{aligned}
\therefore E & =j \frac{z_{0}}{2} \frac{I}{r} \frac{d t}{\lambda} e^{-j k r}\left[e^{j k h \theta o s \theta}-e^{-j k h \cos \theta}\right] \cos \theta \\
& =j \frac{z_{0}}{2} \frac{I}{r} \frac{d t}{\lambda} e^{-j k r} j 2 \sin (k h(\cos \theta) \cos \theta
\end{aligned}
$$

$\because h=2 \lambda$


## principle of pattern multiplication

## Two infinitesimal dipole antennas at XY Plan <br> $$
\Theta=\pi / 2
$$

Case(1)
Infinitesimal oriented along y direction


(a)

(b)

(c)

Case(2)
Infinitesimal oriented along x direction

$$
d=\lambda / 2
$$



(a)

(b)

## LINEAR ARRAY of IDENTICAL ELEMENTS

Controls that can be used to shape the overall pattern of the antenna:

1. The geometrical configuration of the overall array (linear, circular, rectangular, spherical, etc.)
2. The relative displacement between the elements
3. The excitation amplitude of the individual elements
4. The excitation phase of the individual elements
5. The relative pattern of the individual elements


Dipole oriented to y axis

## TWO-ELEMENT ARRAY

For two infinitesimal horizontal dipoles positioned along the $z$-axis Oriented at y axis and suppose we study tot E at YZ plane

$$
\mathbf{E}_{t}=\mathbf{E}_{1}+\mathbf{E}_{2}=\hat{\mathbf{a}}_{\theta} j \eta \frac{k I_{0} l}{4 \pi}\left\{\frac{e^{-j\left[k r_{1}-(\beta / 2)\right]}}{r_{1}} \cos \theta_{1}+\frac{e^{-j\left[k r_{2}+(\beta / 2)\right]}}{r_{2}} \cos \theta_{2}\right\}
$$


(b) Far-field observations

$$
\mathrm{E}_{t}=\hat{\mathrm{a}}_{\theta} j \eta \frac{k I_{0} l e^{-j k r}}{4 \pi r} \cos \theta\left[e^{+j(k d \cos \theta+\beta) / 2}+e^{-j(k d \cos \theta+\beta) / 2}\right]
$$

$$
\mathbf{E}_{t}=\hat{\mathbf{a}}_{\theta} j \eta \frac{k I_{0} l e^{-j k r}}{4 \pi r} \cos \theta\left\{2 \cos \left[\frac{1}{2}(k d \cos \theta+\beta)\right]\right\}
$$

$\mathbf{E}($ total $)=[\mathbf{E}($ single element at reference point $)] \times$ array factor $]$

## Arrays of two isotropic point sources (ARRAY FACTOR PATTERN)

Case 1 same amplitude and phase ( $B=0$ ) and for $d=\lambda / 2 \mathrm{Kd} / 2=\pi / 2$ antennas on az axis (AF) $\mathrm{n}=\boldsymbol{\operatorname { c o s } [ ( k d / 2 ) \operatorname { c o s } \theta ] = \operatorname { c o s } [ ( \pi / 2 ) \operatorname { c o s } \theta ]}$
Max at

$$
\frac{\pi}{2} \cos \theta_{m}=m \pi \quad, \quad m=0,1,2, \ldots \quad \boldsymbol{\theta}_{m}=\cos ^{-1}(0)=\frac{\pi}{2},-\frac{\pi}{2}
$$

Nulls at

$$
\frac{\pi}{2} \cos \theta_{n}= \pm(2 m+1) \pi / 2
$$

$$
\theta_{n}=\cos ^{-1}( \pm 1)=0, \pi
$$



- Case 2 same amplitude and opposite phase $(\beta=180)$ and for $d=\lambda / 2 \mathrm{Kd} / 2=\pi / 2$

$$
\left|(A F)_{n}\right|=\cos \left(\frac{k d}{2} \cos \theta+\pi / 2\right)=\sin \left(\frac{k d}{2} \cos \theta\right)
$$

| $\theta$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $A F_{n}$ | 1 | .999 | .995 | .978 | .933 | .847 | .707 | .5 | .269 | 0 |



Changing phase of source currents shift to 180 change AF pattern as seen in Fig.

- Case 3 (a) same amplitude and quadrature phase $(\beta / 2=\pi / 4)$ and for $d=\lambda / 2$ $\mathrm{Kd} / 2=\pi / 2$

$$
\left|(A F)_{n}\right|=\cos \left(\frac{\pi}{2} \cos \theta+\pi / 4\right)
$$

| $\theta$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\left\|A F_{n}\right\|$ | .707 | .69 | .637 | .543 | .406 | .22 | 0 | .245 | .49 |
| $\theta$ | 90 | 100 | 110 | 120 | 130 | 140 | 150 | 160 | 170 |
| $\left\|A F_{n}\right\|$ | .707 | .87 | .969 | 1 | .975 | .913 | .839 | .77 | .723 |
| $\theta$ | 180 |  |  |  |  |  |  |  |  |
| $\left\|A F_{n}\right\|$ | .707 |  |  |  |  |  |  |  |  |



Most radiation directed toward lower half

- Case 3 (b) same amplitude and quadrature phase ( $\beta / 2=\pi / 4$ ) and for $d=\lambda / 4 K d / 2=\pi / 4$


## Will be described bx phase accumulation

$$
\left|(A F)_{n}\right|=\cos \left(\frac{\pi}{4} \cos \theta+\pi / 4\right)
$$



Can we explain max occurred at 180 and nulls at 0 in terms of phase accumulation of phases Generated by array elements at observation point, ...this illustrated at next slide.

Pattern Synthesis



